https://www.geniustudies.com/download/solutions-manual-engineering-electromagn

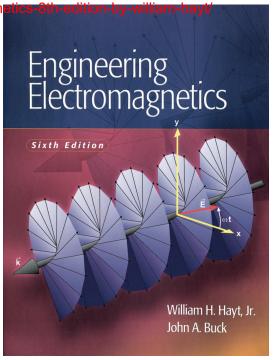
# Interactive e-Text



# Engineering Electromagnetics

Sixth Edition

William H. Hayt, Jr. · John A. Buck





#### **Textbook Table of Contents**

The Textbook Table of Contents is your starting point for accessing pages within the chapter. Once you're at this location, you can easily move back and forth within specific chapters or just as easily jump from one chapter to another.



## **Textbook Website**

The Textbook Website is the McGraw-Hill Higher Education website developed to accompany this textbook. Here you'll find numerous text-specific learning tools and resources that expand upon the information you normally find in a printed textbook.



## **McGraw-Hill Website**

The McGraw-Hill Website is your starting point for discovery of all the educational content and services offered by McGraw-Hill Higher Education.

Copyright @ 2001 The McGraw Companies. All rights reserved. Any use is subject to the Terms of Use and Privacy Policy. McGraw-Hill Higher Education is one of the many fine businesses of The McGraw-Hill Companies.

If you have a question or a suggestion about a specific book or product, please fill out our User Feedback Form accessible from the main menu or contact our customer service line at 1-800-262-4729.

The **McGraw-Hill** Companies



since  $J_x = 0$  there. Current will pass through the three remaining surfaces, and will be found through

$$I = \int_{2}^{3} \int_{0}^{1} \mathbf{J} \cdot (-\mathbf{a}_{y}) \Big|_{y=0} dx dz + \int_{2}^{3} \int_{0}^{1} \mathbf{J} \cdot (\mathbf{a}_{y}) \Big|_{y=1} dx dz + \int_{2}^{3} \int_{0}^{1} \mathbf{J} \cdot (\mathbf{a}_{x}) \Big|_{x=1} dy dz$$

$$= 10^{4} \int_{2}^{3} \int_{0}^{1} \left[ \cos(2x)e^{-0} - \cos(2x)e^{-2} \right] dx dz - 10^{4} \int_{2}^{3} \int_{0}^{1} \sin(2)e^{-2y} dy dz$$

$$= 10^{4} \left( \frac{1}{2} \right) \sin(2x) \Big|_{0}^{1} (3-2) \left[ 1 - e^{-2} \right] + 10^{4} \left( \frac{1}{2} \right) \sin(2)e^{-2y} \Big|_{0}^{1} (3-2) = \underline{0}$$

c) Repeat part b, but use the divergence theorem: We find the net outward current through the surface of the cube by integrating the divergence of  $\mathbf{J}$  over the cube volume. We have

$$\nabla \cdot \mathbf{J} = \frac{\partial J_x}{\partial x} + \frac{\partial J_y}{\partial y} = -10^{-4} \left[ 2\cos(2x)e^{-2y} - 2\cos(2x)e^{-2y} \right] = \underline{0} \text{ as expected}$$

- 5.11. Two perfectly-conducting cylindrical surfaces are located at  $\rho = 3$  and  $\rho = 5$  cm. The total current passing radially outward through the medium between the cylinders is 3 A dc. Assume the cylinders are both of length l.
  - a) Find the voltage and resistance between the cylinders, and **E** in the region between the cylinders, if a conducting material having  $\sigma = 0.05 \, \text{S/m}$  is present for  $3 < \rho < 5 \, \text{cm}$ : Given the current, and knowing that it is radially-directed, we find the current density by dividing it by the area of a cylinder of radius  $\rho$  and length l:

$$\mathbf{J} = \frac{3}{2\pi\rho l} \, \mathbf{a}_{\rho} \, \, \mathrm{A/m^2}$$

Then the electric field is found by dividing this result by  $\sigma$ :

$$\mathbf{E} = \frac{3}{2\pi\sigma\rho l}\,\mathbf{a}_\rho = \frac{9.55}{\rho l}\mathbf{a}_\rho \,\,\mathrm{V/m}$$

The voltage between cylinders is now:

$$V = -\int_5^3 \mathbf{E} \cdot \mathbf{dL} = \int_3^5 \frac{9.55}{\rho l} \mathbf{a}_\rho \cdot \mathbf{a}_\rho d\rho = \frac{9.55}{l} \ln\left(\frac{5}{3}\right) = \frac{4.88}{l} \text{ V}$$

Now, the resistance will be

$$R = \frac{V}{I} = \frac{4.88}{3l} = \frac{1.63}{l} \ \Omega$$

b) Show that integrating the power dissipated per unit volume over the volume gives the total dissipated power: We calculate

$$P = \int_{v} \mathbf{E} \cdot \mathbf{J} \, dv = \int_{0}^{l} \int_{0}^{2\pi} \int_{.03}^{.05} \frac{3^{2}}{(2\pi)^{2} \rho^{2} (.05) l^{2}} \, \rho \, d\rho \, d\phi \, dz = \frac{3^{2}}{2\pi (.05) l} \ln \left( \frac{5}{3} \right) = \frac{14.64}{l} \, \mathbf{W}$$

We also find the power by taking the product of voltage and current:

$$P = VI = \frac{4.88}{l}(3) = \frac{14.64}{l} W$$

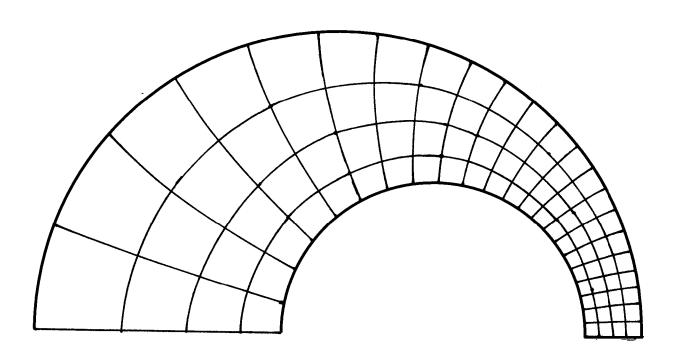
6.3. Construct a curvilinear square map of the potential field between two parallel circular cylinders, one of 4-cm radius inside one of 8-cm radius. The two axes are displaced by 2.5 cm. These dimensions are suitable for the drawing. As a check on the accuracy, compute the capacitance per meter from the sketch and from the exact expression:

$$C = \frac{2\pi\epsilon}{\cosh^{-1}\left[(a^2 + b^2 - D^2)/(2ab)\right]}$$

where a and b are the conductor radii and D is the axis separation.

Our attempt at the drawing is shown below. Use of the exact expression above yields a capacitance value of  $C = 11.5\epsilon_0$  F/m. Use of the drawing produces:

$$C \doteq \frac{22 \times 2}{4} \epsilon_0 = \underline{11\epsilon_0 \text{ F/m}}$$



10.17. (continued) Now

$$\mathbf{E} = \frac{\mathbf{D}}{\epsilon_0} = \int \frac{1}{\epsilon_0} \nabla \times \mathbf{H} \ dt + C_2 = \frac{C(144 + a^2)}{\mu_0 \epsilon_0 (2 \times 10^{10})^2} \sin(12y) \sin(az) \cos(2 \times 10^{10}t) \, \mathbf{a}_x$$

where  $C_2 = 0$ . This field must be the same as the original field as stated, and so we require that

$$\frac{C(144 + a^2)}{\mu_0 \epsilon_0 (2 \times 10^{10})^2} = 1$$

Using  $\mu_0 \epsilon_0 = (3 \times 10^8)^{-2}$ , we find

$$a = \left[ \frac{(2 \times 10^{10})^2}{(3 \times 10^8)^2} - 144 \right]^{1/2} = \underline{66}$$

11.7. The phasor magnetic field intensity for a 400-MHz uniform plane wave propagating in a certain lossless material is  $(2\mathbf{a}_y - j5\mathbf{a}_z)e^{-j25x}$  A/m. Knowing that the maximum amplitude of  $\mathbf{E}$  is 1500 V/m, find  $\beta$ ,  $\eta$ ,  $\lambda$ ,  $v_p$ ,  $\epsilon_R$ ,  $\mu_R$ , and  $\mathbf{H}(x,y,z,t)$ : First, from the phasor expression, we identify  $\beta = \underline{25 \text{ m}^{-1}}$  from the argument of the exponential function. Next, we evaluate  $H_0 = |\mathbf{H}| = \sqrt{\mathbf{H} \cdot \mathbf{H}^*} = \sqrt{2^2 + 5^2} = \sqrt{29}$ . Then  $\eta = E_0/H_0 = 1500/\sqrt{29} = \underline{278.5~\Omega}$ . Then  $\lambda = 2\pi/\beta = 2\pi/25 = .25~\mathrm{m} = \underline{25~\mathrm{cm}}$ . Next,

$$v_p = \frac{\omega}{\beta} = \frac{2\pi \times 400 \times 10^6}{25} = \underline{1.01 \times 10^8 \text{ m/s}}$$

Now we note that

$$\eta = 278.5 = 377 \sqrt{\frac{\mu_R}{\epsilon_R}} \quad \Rightarrow \quad \frac{\mu_R}{\epsilon_R} = 0.546$$

And

$$v_p = 1.01 \times 10^8 = \frac{c}{\sqrt{\mu_R \epsilon_R}} \quad \Rightarrow \quad \mu_R \epsilon_R = 8.79$$

We solve the above two equations simultaneously to find  $\epsilon_R = \underline{4.01}$  and  $\mu_R = \underline{2.19}$ . Finally,

$$\mathbf{H}(x, y, z, t) = Re \left\{ (2\mathbf{a}_y - j5\mathbf{a}_z)e^{-j25x}e^{j\omega t} \right\}$$
  
=  $2\cos(2\pi \times 400 \times 10^6 t - 25x)\mathbf{a}_y + 5\sin(2\pi \times 400 \times 10^6 t - 25x)\mathbf{a}_z \text{ A/m}$ 

- 11.15. A 10 GHz radar signal may be represented as a uniform plane wave in a sufficiently small region. Calculate the wavelength in centimeters and the attenuation in nepers per meter if the wave is propagating in a non-magnetic material for which
  - a)  $\epsilon_R' = 1$  and  $\epsilon_R'' = 0$ : In a non-magnetic material, we would have:

$$\alpha = \omega \sqrt{\frac{\mu_0 \epsilon_0 \epsilon_R'}{2}} \left[ \sqrt{1 + \left(\frac{\epsilon_R''}{\epsilon_R'}\right)^2} - 1 \right]^{1/2}$$

and

$$\beta = \omega \sqrt{\frac{\mu_0 \epsilon_0 \epsilon_R'}{2}} \left[ \sqrt{1 + \left(\frac{\epsilon_R''}{\epsilon_R'}\right)^2} + 1 \right]^{1/2}$$

With the given values of  $\epsilon_R'$  and  $\epsilon_R''$ , it is clear that  $\beta = \omega \sqrt{\mu_0 \epsilon_0} = \omega/c$ , and so  $\lambda = 2\pi/\beta = 2\pi c/\omega = 3 \times 10^{10}/10^{10} = \underline{3}$  cm. It is also clear that  $\alpha = \underline{0}$ .